Systems Engineering/Process Control L3

- Mathematical modeling
- State-space models
- Stability

Reading: Systems Engineering and Process Control: 3.1-3.4

Process modeling

- Dynamics in processes often described by differential equations
- Two approaches:
 - 1. Mathematical modeling
 - Use physical laws (conservation equations etc) to create model
 - 2. Experiments
 - Create experiments (e.g., step response), analyze input & output
 - FRT041 System identification

In practice, a combination of both methods is often used

Mathematical modeling

- Flow balances
- Intensity balances
- Constitutive relations

Flow balances

volume flow [m³/s]

material flow (mass balance) [mol/s]

 $\begin{bmatrix} Change in number of \\ accumulated particles \\ per time unit \end{bmatrix} = \begin{bmatrix} Inflow of \\ particles \end{bmatrix} - \begin{bmatrix} Outflow of \\ particles \end{bmatrix}$

Flow balances

energy flow [W]

current flow [A]

$$\begin{bmatrix} Sum \ current \\ to \ node \end{bmatrix} = \begin{bmatrix} Sum \ current \\ from \ node \end{bmatrix}$$

Intensity balances

momentum balance [N]

$$\begin{bmatrix} Change in \\ momentum \\ per time unit \end{bmatrix} = \begin{bmatrix} Driving \\ forces \end{bmatrix} - \begin{bmatrix} Braking \\ forces \end{bmatrix}$$

voltage balance [V]

[Sum voltage around circuit] = 0

Constitutional relations

Ideal gas law

$$p = \frac{nR}{V}T$$

Torricelli's law

$$v = \sqrt{2gh}$$

Energy in heated liquid

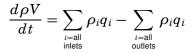
$$W = C_p \rho V T$$

Ohm's law

$$u = Ri$$

Typical balance equations for chemical processes

Total mass balance:



Mass balance for component *j*:

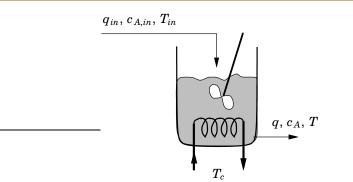
$$\frac{dc_j V}{dt} = \sum_{\substack{i = \text{all} \\ \text{inlets}}} c_{j,i} q_i - \sum_{\substack{i = \text{all} \\ \text{outlets}}} c_{j,i} q_i + r_j V$$

Total energy balance:



(all follow from physical conservation laws)

Example: CSTR with exothermic reaction



- Exothermic reaction $A \rightarrow B$, $r = k_0 e^{-E/RT} c_A$
- Cooling coil with temperature T_c
- Perfect stirring, constant density ρ

Example: CSTR with exothermic reaction

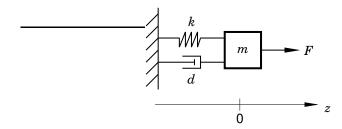
Total mass balance, balance for comp. A, and total energy balance:

$$\begin{aligned} \frac{dV}{dt} &= q_{in} - q\\ \frac{dc_A}{dt} &= \frac{q_{in}}{V}(c_{A,in} - c_A) - k_0 e^{-E/RT} c_A\\ \frac{dT}{dt} &= \frac{q_{in}}{V}(T_{in} - T) + \frac{(-\Delta H_r)k_0}{\rho C_p} e^{-E/RT} c_A + \frac{UA}{V\rho C_p}(T_c - T) \end{aligned}$$

after simplifications

- Nonlinear third order model
- ▶ State variables: V, c_A, T
- ▶ Possible inputs: q_{in} , q, $c_{A,in}$, T_{in} , T_c
- ▶ Parameters (constants): ρ , C_p , $(-\Delta H_r)$, k_0 , E, R, U, A

Example: Mechanical system



- Mass m with position z
- External force: F
- Spring force: $F_k = -kz$
- Damper force: $F_d = -d\dot{z}$

Example: Mechanical system

Momentum balance:

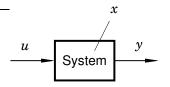
$$m\ddot{z} = F - kz - d\dot{z}$$

Introduce $v = \dot{z} \Rightarrow$

$$\dot{v} = -\frac{d}{m}v - \frac{k}{m}z + \frac{1}{m}F$$
$$\dot{z} = v$$

- Linear second order model
- State variables v, z
- Input: F
- ▶ Parameters (constants): *m*, *k*, *d*

State-space form



In general, x, u and y are vectors:

$$x = \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} \quad u = \begin{pmatrix} u_1 \\ \vdots \\ u_m \end{pmatrix} \quad y = \begin{pmatrix} y_1 \\ \vdots \\ y_p \end{pmatrix}$$

- n = number of state variables = system order
- m = number of inputs
- p = number of outputs (measurements)

State-space form

- x is called system state (state)
 - it contains values of all accumulated quantities in the system
 - (it represents the system "memory")
- The dynamics are described by n first order differential equations:

$$\frac{dx_1}{dt} = f_1(x_1, \ldots, x_n, u_1, \ldots, u_m)$$

$$\vdots$$

$$\frac{dx_n}{dt} = f_n(x_1, \ldots, x_n, u_1, \ldots, u_m)$$

State-space form

Outputs described by p algebraic equations (not always stated):

$$y_1 = g_1(x_1, ..., x_n, u_1, ..., u_m)$$

 \vdots
 $y_p = g_p(x_1, ..., x_n, u_1, ..., u_m)$

System can be written in vector form as:

$$rac{dx}{dt} = f(x, u)$$
 (state equation)
 $y = g(x, u)$ (measurement equation)

▶ (*f* and *g* can be nonlinear functions)

State-space form for linear systems

- A system is linear if all f_i and g_i are linear functions
- Example:

$$\frac{dx_1}{dt} = a_{11}x_1 + \dots + a_{1n}x_n + b_{11}u_1 + \dots + b_{1m}u_m$$

$$\vdots$$

$$\frac{dx_n}{dt} = a_{n1}x_1 + \dots + a_{nn}x_n + b_{n1}u_1 + \dots + b_{nm}u_m$$

$$y_1 = c_{11}x_1 + \dots + c_{1n}x_n + d_{11}u_1 + \dots + d_{1m}u_m$$

$$\vdots$$

$$y_p = c_{p1}x_1 + \dots + c_{pn}x_n + d_{p1}u_1 + \dots + d_{pm}u_m$$

State space form for linear systems

In matrix form:

$$\frac{dx}{dt} = Ax + Bu$$
 (state equation)
 $y = Cx + Du$ (measurement equation)

- x and u are deviations from equilibrium point
- (x, u) = (0, 0) is always in equilibrium (why?)
- D is called system direct term (often 0 for real processes)

Mini problem: What dimensions does matrices A, B, C and D have?

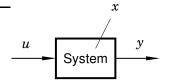
Example: Mechanical system

State vector:
$$x = \begin{pmatrix} v \\ z \end{pmatrix}$$

- We control u = F and measure y = z
- The model on state space form with matrices:

$$\frac{dx}{dt} = \underbrace{\begin{pmatrix} -\frac{d}{m} & -\frac{k}{m} \\ 1 & 0 \end{pmatrix}}_{A} x + \underbrace{\begin{pmatrix} \frac{1}{m} \\ 0 \end{pmatrix}}_{B} u$$
$$y = \underbrace{\begin{pmatrix} 0 & 1 \\ C \end{pmatrix}}_{C} x + \underbrace{\begin{pmatrix} 0 \\ 0 \end{pmatrix}}_{D} u$$

Solution of the linear state equation



state-space model of system:

$$\frac{dx}{dt} = Ax + Bu$$
 (state equation)
$$y = Cx + Du$$
 (measurement equation)

• How does x (and y) depend on input u and initial state x(0)?

Solution of state equation – scalar case

System with one state variable and one input:

$$\frac{dx(t)}{dt} = ax(t) + bu(t)$$

Solution:

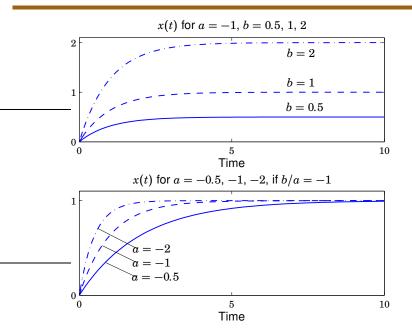
$$x(t) = e^{at}x(0) + \int_0^t e^{a(t-\tau)}bu(\tau)\,d\tau$$

• Example: Constant input $u(t) = u_0$ and $a \neq 0$:

$$x(t) = e^{at}x(0) + \frac{b}{a}(e^{at} - 1)u_0$$

x(t) limited if a < 0

Simulation with u(t) = 1 and x(0) = 0



Solution of state equation – general case

State space model:

$$\frac{dx}{dt} = Ax + Bu$$

Solution:

$$x(t) = e^{At}x(0) + \int_0^t e^{A(t-\tau)}Bu(\tau) d\tau$$

where e^{At} is matrix exponential function, defined as

$$e^{At} = I + At + \frac{(At)^2}{2!} + \frac{(At)^3}{3!} + \cdots$$

Example: Mechanical system

Recall state-space system:

$$\frac{dx}{dt} = \begin{pmatrix} -\frac{d}{m} & -\frac{k}{m} \\ 1 & 0 \end{pmatrix} x + \begin{pmatrix} \frac{1}{m} \\ 0 \end{pmatrix} u$$

Assume:

$$d = 0, \quad F = u = 0, \quad x(0) = \begin{pmatrix} v(0) \\ z(0) \end{pmatrix} = \begin{pmatrix} 0 \\ 1 \end{pmatrix}, \quad m = k = 1$$

i.e., no damping, no external force

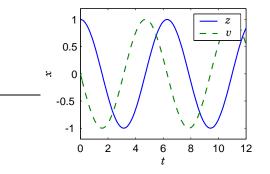
Gives state-space system and exponential matrix:

$$\frac{dx}{dt} = \underbrace{\begin{pmatrix} 0 & -1\\ 1 & 0 \end{pmatrix}}_{A} x, \qquad e^{At} = \begin{pmatrix} \cos t & -\sin t\\ \sin t & \cos t \end{pmatrix}$$

Solution:

$$x(t) = e^{At}x(0) = \begin{pmatrix} \cos t & -\sin t \\ \sin t & \cos t \end{pmatrix} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} -\sin t \\ \cos t \end{pmatrix}$$

Simulation of mechanical system



Eigenvalues

▶ Eigenvalues of *A* given by *n* roots to characteristic equation:

 $\det(\lambda I - A) = 0$

- $det(\lambda I A) = P(\lambda)$ is called characteristic polynomial
- Eigenvalues can be complex
- Multiplicity of eigenvalue = nbr of eigenvalues with same value

Eigenvalues

Suppose A is diagonal with eigenvalues $\lambda_1, \ldots, \lambda_n$:

$$A = \begin{pmatrix} \lambda_1 & 0 & 0 & \dots & 0 \\ 0 & \lambda_2 & 0 & \dots & 0 \\ \vdots & & \ddots & \vdots \\ 0 & 0 & 0 & \dots & \lambda_n \end{pmatrix}$$

Then

$$e^{At} = \begin{pmatrix} e^{\lambda_1 t} & 0 & 0 & \dots & 0 \\ 0 & e^{\lambda_2 t} & 0 & \dots & 0 \\ \vdots & & \ddots & \vdots \\ 0 & 0 & 0 & \dots & e^{\lambda_n t} \end{pmatrix}$$

• Every eigenvalue λ_i gives a term $e^{\lambda_i t}$ in solution

Eigenvalues

- Assume that A is a general matrix
- Every eigenvalue of A gives a term $P_{m_i-1}(t)e^{\lambda_i t}$ in e^{At} where
 - $P_{m_i-1}(t)$ is a polynomial in t of order at most $m_i 1$
 - *m_i* is the multiplicity of the eigenvalue
- Example: A mat

A matrix
$$A = \begin{pmatrix} -1 & 1 \\ 0 & -1 \end{pmatrix}$$

Eigenvalues:

$$\lambda_1=\lambda_2=-1 \quad (m=2)$$

Exponential matrix:

$$e^{At} = egin{pmatrix} e^{-t} & te^{-t} \ 0 & e^{-t} \end{bmatrix}$$

- Stability is a system property does not depend on input
- Can therefore study the uncontrolled system:

$$\frac{dx}{dt} = Ax$$

Solution:

$$x(t) = e^{At}x(0)$$

Stability notions

Asymptotic stability: $x(t) \to 0$ as $t \to \infty$ for all initial states **Stability**: x(t) limited as $t \to \infty$ for all initial states **Instability**: x(t) unlimited as $t \to \infty$ for some initial state

(Marginally stable: Stable but not asymptotically stable system)

Example

Asymptotically stable systems:

- Water tank with hole in the bottom
- Temperature in oven
- Speed in a car

(Marginally) Stable systems:

- Water tank without hole in the bottom
- Mass-damper-spring system without damping
- Distance covered in a car

Unstable systems:

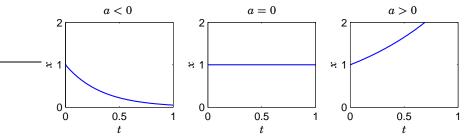
- Inverted pendulum
- Segway

Stability in the scalar case

State-space model and solution:

$$\frac{dx(t)}{dt} = ax(t), \qquad \qquad x(t) = e^{at}x(0)$$

Solution plots for different a:



- asymptotically stable if a < 0
- stable if $a \leq 0$
- unstable if a > 0

Stability in the general case

- Eigenvalues λ_i to A-matrix decides stability
- A linear system is:
 - Asymptotically stable if all $\operatorname{Re}(\lambda_i) < 0$
 - Unstable if some $\operatorname{Re}(\lambda_i) > 0$
 - Stable if all Re(λ_i) ≤ 0 and possible pure imaginary eigenvalues have multiplicity 1

Routh–Hurwitz stability criteria

Second order systems:

> 2nd order characteristic polynomial (for 2×2 -matrix A):

$$\det(\lambda I - A) = P(\lambda) = \lambda^2 + p_1\lambda + p_2$$

► All roots in left half-plane (all $\operatorname{Re}(\lambda_i) < 0$) iff $p_1 > 0$ and $p_2 > 0$

Third order systems:

▶ 3rd order characteristic polynomial (for 3×3 -matrix A):

$$\det(\lambda I - A) = P(\lambda) = \lambda^3 + p_1 \lambda^2 + p_2 \lambda + p_3$$

All roots in left half-plane iff $p_1 > 0$, $p_2 > 0$, $p_3 > 0$ and $p_1p_2 > p_3$.

Example: Mechanical system

State-space model:

$$\frac{dx}{dt} = \begin{pmatrix} -\frac{d}{m} & -\frac{k}{m} \\ 1 & 0 \end{pmatrix} x + \begin{pmatrix} \frac{1}{m} \\ 0 \end{pmatrix} u$$
$$y = \begin{pmatrix} 0 & 1 \end{pmatrix} x$$

Characteristic equation:

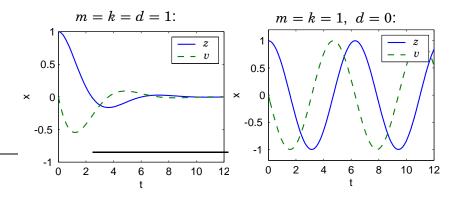
$$\det(\lambda I - A) = egin{bmatrix} \lambda + rac{d}{m} & rac{k}{m} \ -1 & \lambda \end{bmatrix} = \lambda^2 + rac{d}{m}\lambda + rac{k}{m} = 0$$

- Suppose m, k, d > 0: Asymptotically stable
- Suppose m, k > 0, d = 0: Eigenvalues

$$\lambda_{1,2} = \pm i \sqrt{\frac{k}{m}}$$

stable (but not asymptotically stable)

Simulation of mechanical system



Linear systems on state-space form in MATLAB

```
% Define system matrices
A = [1 2; 3 4];
B = [0; 1];
C = [1 \ 0];
D = 0;
% Create state-space model
sys = ss(A, B, C, D);
% Compute eigenvalues to A matrix
eiq(A)
```

% Simulate system w/o input from initial state x0
initial(sys,x0)