Step Response Analysis. Frequency Response, Relation Between Model Descriptions

Automatic Control, Basic Course, Lecture 3

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Content

1. Step Response Analysis
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Step Response Analysis

Steup Response

From the last lecture, we know that if the input $u(t)$ is a step, then the output in the Laplace domain is

$$Y(s) = G(s)U(s) = G(s)\frac{1}{s}$$

It is possible to do an inverse transform of $Y(s)$ to get $y(t)$, but is it possible to claim things about $y(t)$ by only studying $Y(s)$?

We will study how the poles affects the step response. (The zeros will be discussed later)

Initial and Final Value Theorem

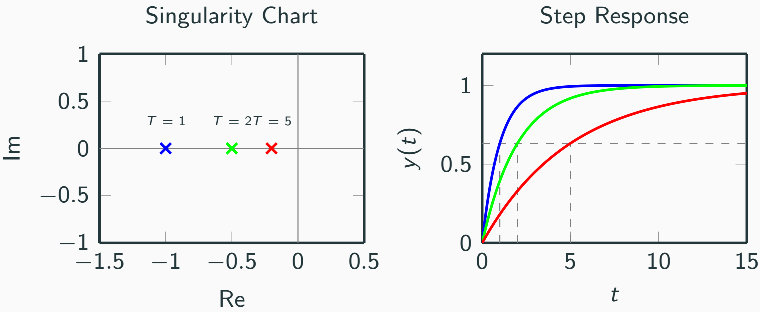
Let $F(s)$ be the Laplace transformation of $f(t)$, i.e., $F(s) = \mathcal{L}(f(t))(s)$.
Given that the limits below exist, it holds that:

Initial value theorem	$\lim_{t \to 0} f(t) = \lim_{s \to +\infty} sF(s)$
Final value theorem	$\lim_{t \to +\infty} f(t) = \lim_{s \to 0} sF(s)$

For a step response we have that:

$$\lim_{t \to +\infty} y(t) = \lim_{s \to 0} sY(s) = \lim_{s \to 0} sG(s)\frac{1}{s} = G(0)$$

First Order System



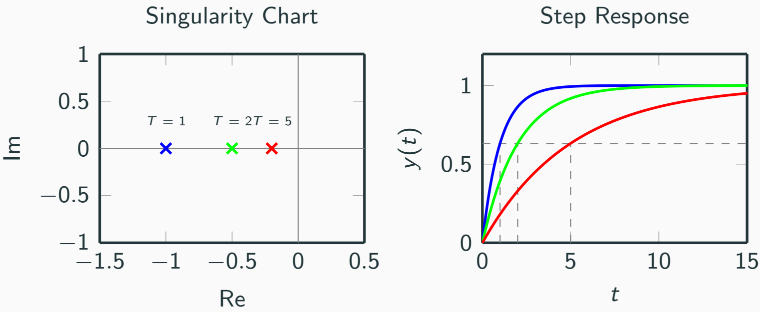
$$G(s) = \frac{K}{1 + sT}$$

One pole in $s = -1/T$

Step response:

$$Y(s) = G(s)\frac{1}{s} = \frac{K}{s(1+sT)} \quad \xrightarrow{\mathcal{L}^{-1}} \quad y(t) = K\left(1 - e^{-t/T}\right)$$

First Order System

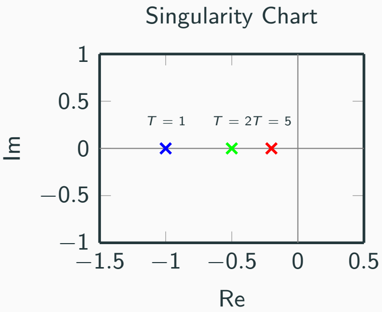


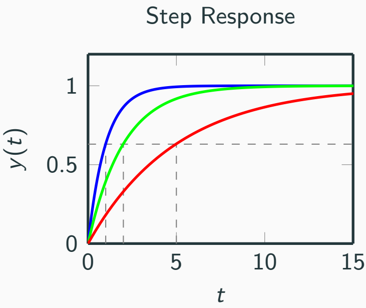
$$G(s) = \frac{K}{1 + sT}$$

Final value:

$$\lim_{t \to +\infty} y(t) = \lim_{s \to 0} sY(s) = \lim_{s \to 0} \frac{K}{s(1 + sT)} = K$$

First Order System





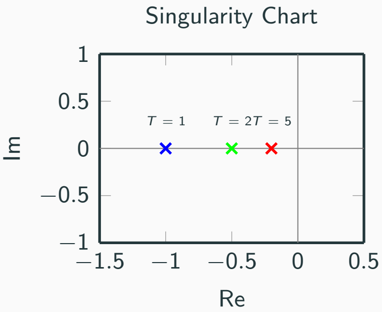
$$G(s) = \frac{K}{1 + sT}$$

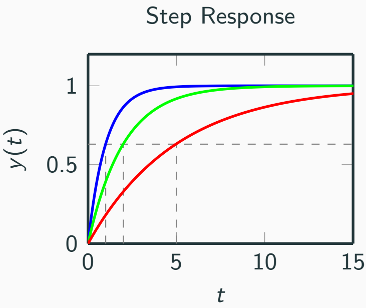
T is called the time-constant:

$$y(T) = K(1 - e^{-T/T}) = K(1 - e^{-1}) \approx 0.63K$$

I.e., T is time it takes for the step response to reach 63% of its final value

First Order System



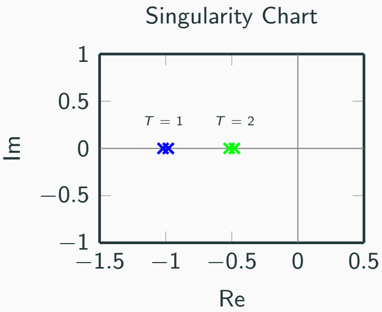


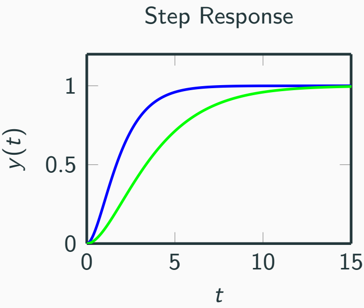
$$G(s) = \frac{K}{1 + sT}$$

Derivative at zero:

$$\lim_{t \to 0} \dot{y}(t) = \lim_{s \to +\infty} s \cdot sY(s) = \lim_{s \to +\infty} \frac{s^2 K}{s(1 + sT)} = \frac{K}{T}$$

Second Order System With Real Poles



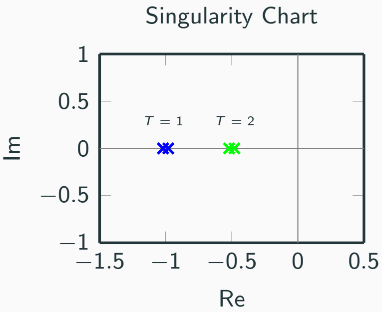


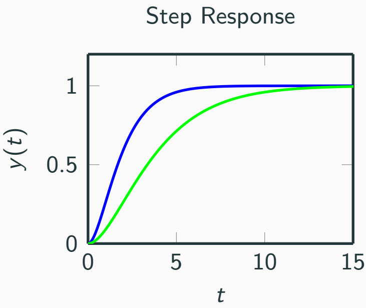
$$G(s) = \frac{K}{(1+sT_1)(1+sT_2)}$$

Poles in $s = -1/T_1$ and $s = -1/T_2$. Step response:

$$y(t) = \begin{cases} K\left(1 - \frac{T_1 e^{-t/T_1} - T_2 e^{-t/T_2}}{T_1 - T_2}\right) & T_1 \neq T_2 \\ K\left(1 - e^{-t/T} - \frac{t}{T} e^{-t/T}\right) & T_1 = T_2 = T \end{cases}$$

Second Order System With Real Poles



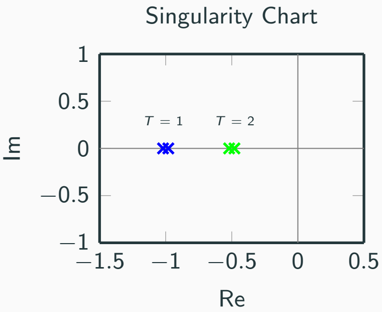


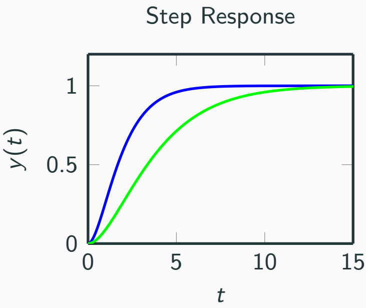
$$G(s) = \frac{K}{(1 + sT_1)(1 + sT_2)}$$

Final value:

$$\lim_{t \to +\infty} = \lim_{s \to 0} sY(s) = \lim_{s \to 0} \frac{sK}{s(1 + sT_1)(1 + sT_2)} = K$$

Second Order System With Real Poles





$$G(s) = \frac{K}{(1 + sT_1)(1 + sT_2)}$$

Derivative at zero:

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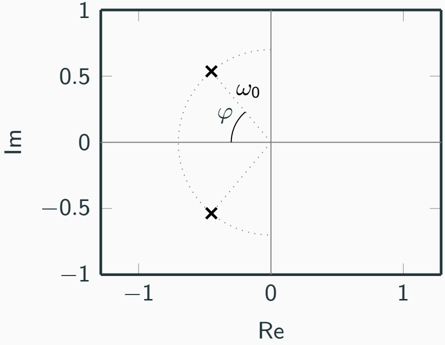
Second Order System With Complex Poles

$$G(s) = \frac{K\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}, \quad 0 < \zeta < 1$$

Relative damping ζ, related to the angle φ

$$\zeta = \cos(\varphi)$$

Singularity Chart



Second Order System With Complex Poles

$$G(s) = \frac{K\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}, \quad 0 < \zeta < 1$$

Inverse transformation yields:

$$y(t) = K\left(1 - \frac{1}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_0 t} \sin\left(\omega_0\sqrt{1-\zeta^2}\,t + \arccos\zeta\right)\right)$$

Second Order System With Complex Poles

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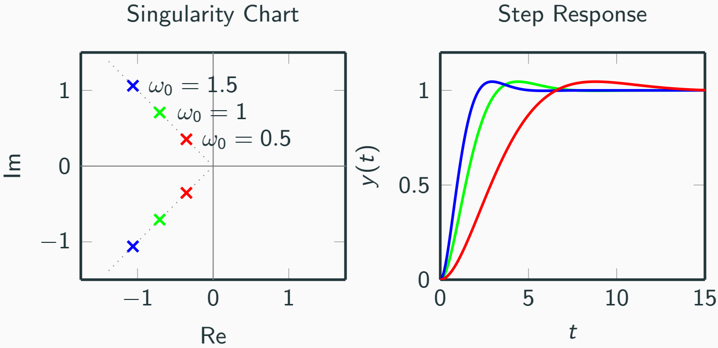

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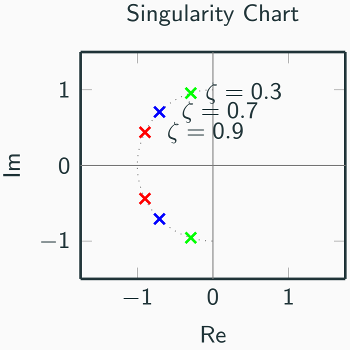
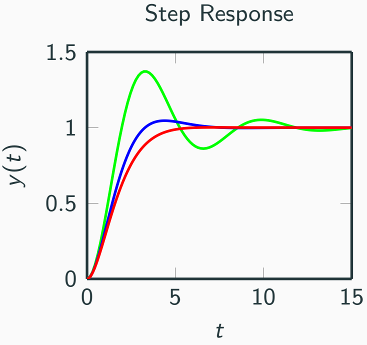
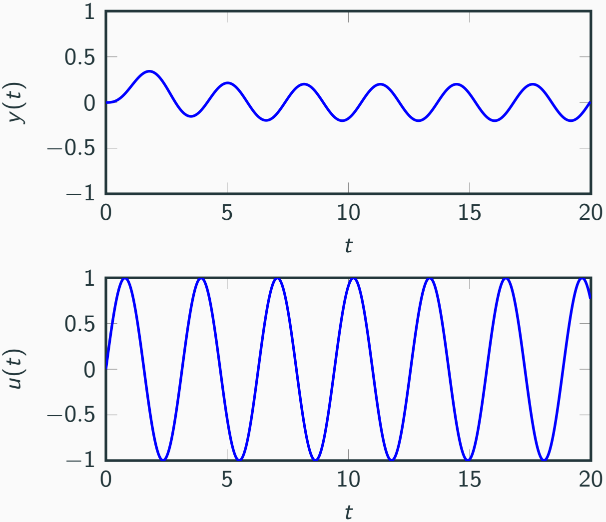




Frequency Response

Sinusoidial Input

Given a transfer function $G(s)$, what happens if we let the input be $u(t) = \sin(\omega t)$?



Sinusoidial Input

It can be shown that if the input is $u(t) = \sin(\omega t)$, the output will be

$$y(t) = a \sin(\omega t + \varphi)$$

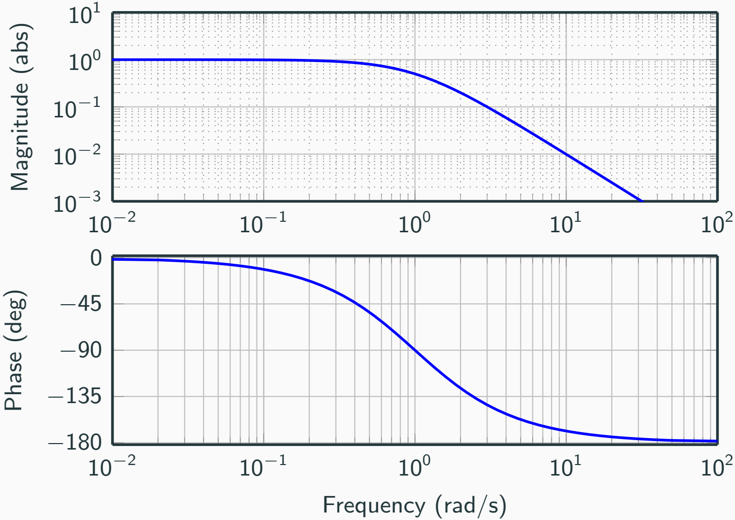
where

$$a = |G(i\omega)|$$
$$\varphi = \arg G(i\omega)$$

So if we determine a and φ for different frequencies, we have a description of the transfer function.

Bode Plot

Idea: Plot $|G(i\omega)|$ and $\arg G(i\omega)$ for different frequencies ω.



Bode Plot - Products of Transfer Functions

Let

$$G(s) = G_1(s)G_2(s)G_3(s)$$

then

$$\begin{aligned} \log|G(i\omega)| &= \log|G_1(i\omega)| + \log|G_2(i\omega)| + \log|G_3(i\omega)| \\ \arg G(i\omega) &= \arg G_1(i\omega) + \arg G_2(i\omega) + \arg G_3(i\omega) \end{aligned}$$

This means that we can construct Bode plots of transfer functions from simple "building blocks" for which we know the Bode plots.

Bode Plot of $G(s) = K$

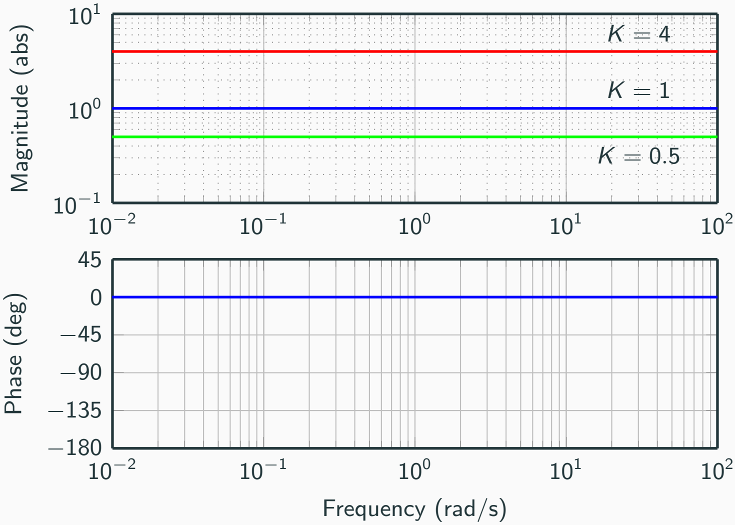
If

$$G(s) = K$$

then

$$\log|G(i\omega)| = \log(K)$$
$$\arg G(i\omega) = 0$$

Bode Plot of $G(s) = K$



Bode Plot of $G(s) = s^n$

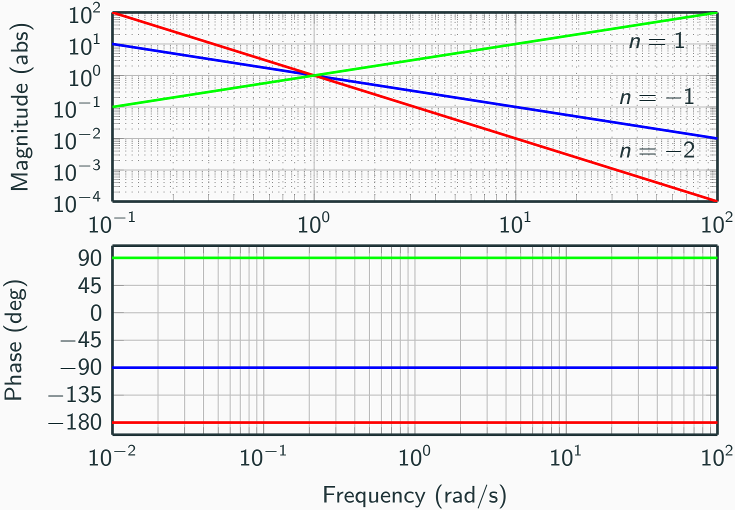
If

$$G(s) = s^n$$

then

$$\log|G(i\omega)| = n\log(\omega)$$
$$\arg G(i\omega) = n\frac{\pi}{2}$$

Bode Plot of $G(s) = s^n$



Bode Plot of $G(s) = (1 + sT)^n$

If

$$G(s) = (1 + sT)^n$$

then

$$\log|G(i\omega)| = n\log(\sqrt{1 + \omega^2 T^2})$$
$$\arg G(i\omega) = n\arg(1 + i\omega T) = n\arctan(\omega T)$$

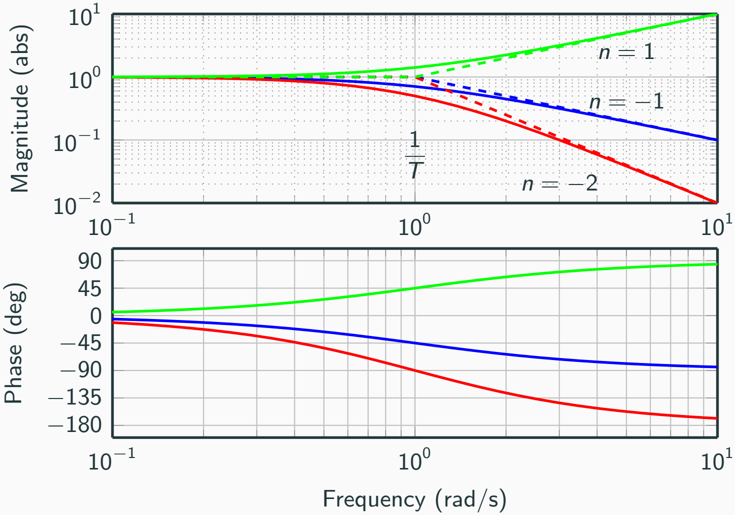
For small ω

$$\log|G(i\omega)| \to 0$$
$$\arg G(i\omega) \to 0$$

For large ω

$$\log|G(i\omega)| \to n\log(\omega T)$$
$$\arg G(i\omega) \to n\frac{\pi}{2}$$

Bode Plot of $G(s) = (1 + sT)^n$



Bode Plot of $G(s) = (1 + 2\zeta s/\omega_0 + (s/\omega_0)^2)^n$

$$G(s) = (1 + 2\zeta s/\omega_0 + (s/\omega_0)^2)^n$$

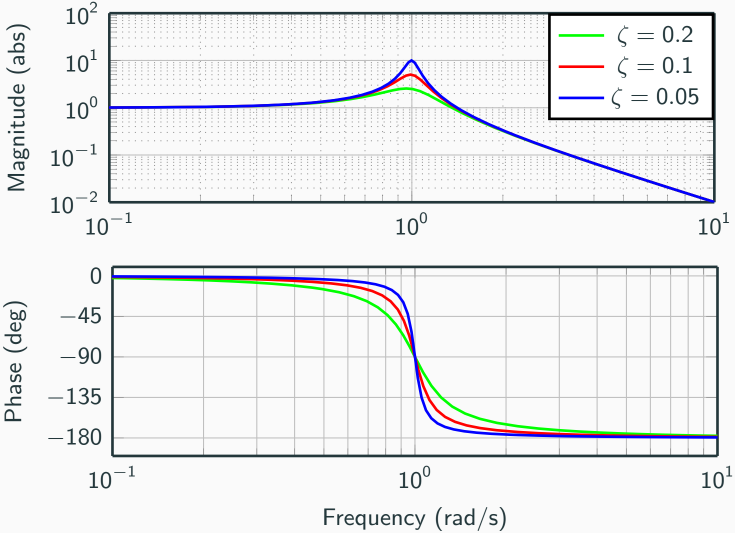
For small ω

$$\log|G(i\omega)| \to 0$$
$$\arg(i\omega) \to 0$$

For large ω

$$\log|G(i\omega)| \to 2n \log\left(\frac{\omega}{\omega_0}\right)$$
$$\arg G(i\omega) \to n\pi$$

Bode Plot of $G(s) = (1 + 2\zeta s/\omega_0 + (s/\omega_0)^2)^n$



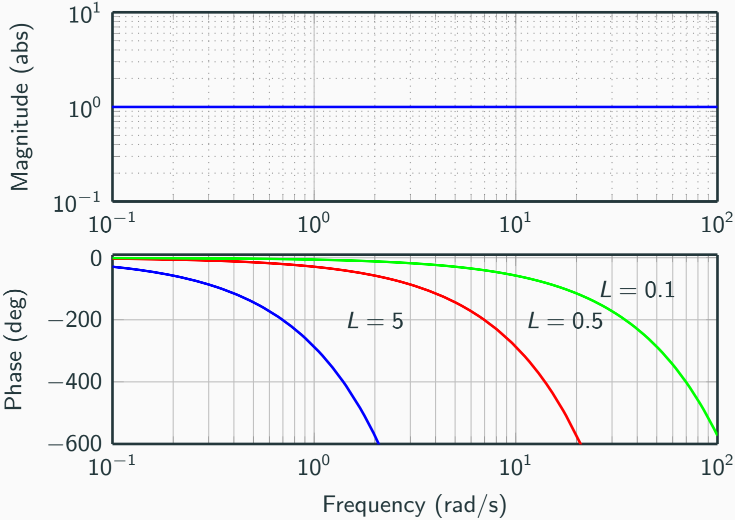
Bode Plot of $G(s) = e^{-sL}$

$$G(s) = e^{-sL}$$

Describes a pure time delay with delay L, i.e, $y(t) = u(t - L)$

$$\log |G(i\omega)| = 0$$
$$\arg G(i\omega) = -\omega L$$

Bode Plot of $G(s) = e^{-sL}$



Bode Plot of Composite Transfer Function

Example

Draw the Bode plot of the transfer function

$$G(s) = \frac{100(s+2)}{s(s+20)^2}$$

First step, write it as product of sample transfer functions:

$$G(s) = \frac{100(s+2)}{s(s+20)^2} = 0.5 \cdot s^{-1} \cdot (1+0.5s) \cdot (1+0.05s)^{-2}$$

Then determine the corner frequencies:

$$G(s) = \frac{100(s+2)}{s(s+20)^2} = 0.5 \cdot s^{-1} \cdot \overbrace{(1+0.5s)}^{w_{c_1}=2} \cdot \overbrace{(1+0.05s)^{-2}}^{w_{c_2}=20}$$

Bode Plot of Composite Transfer Function

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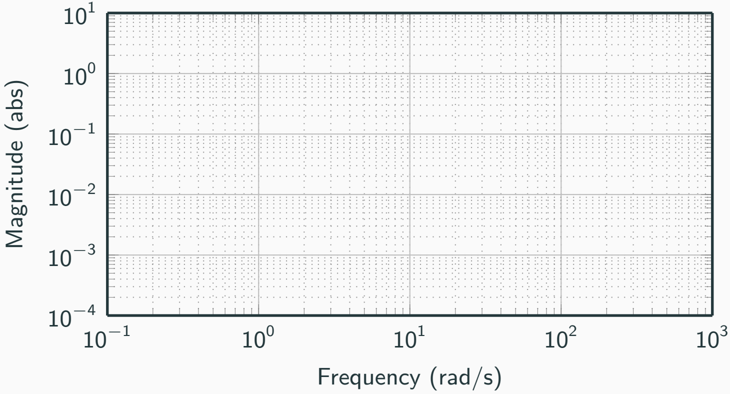

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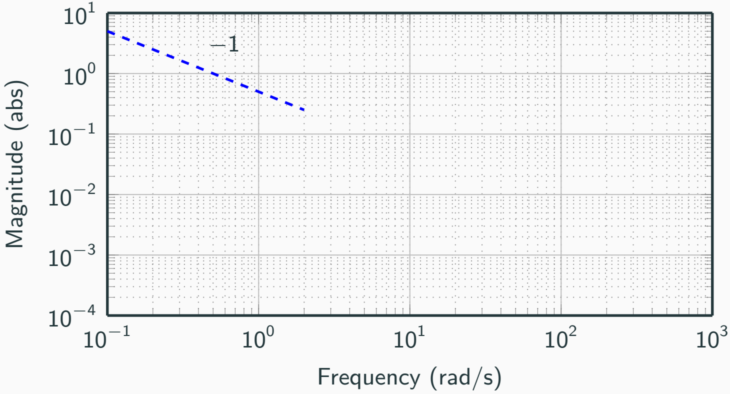

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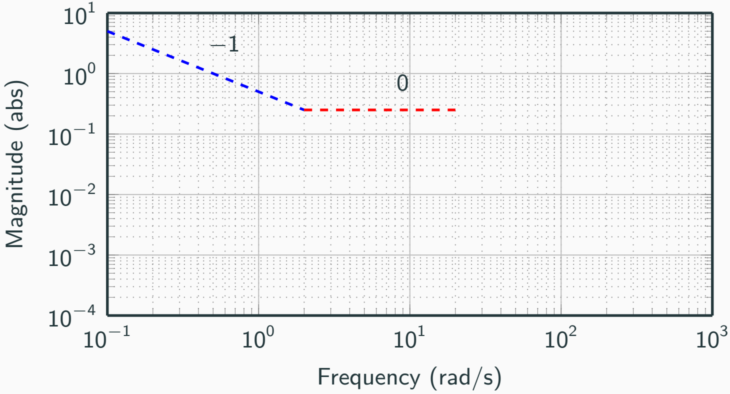

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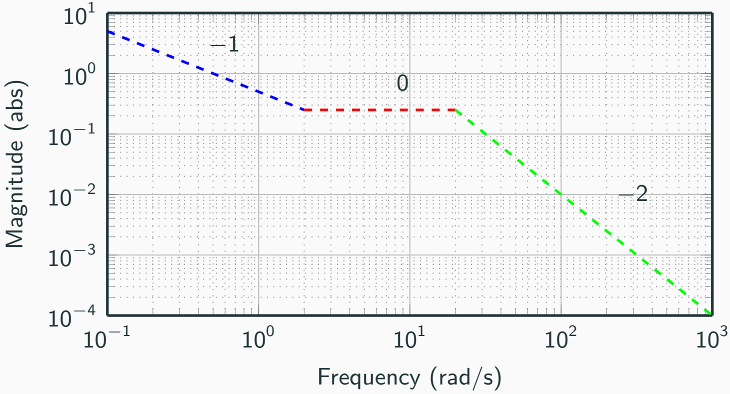

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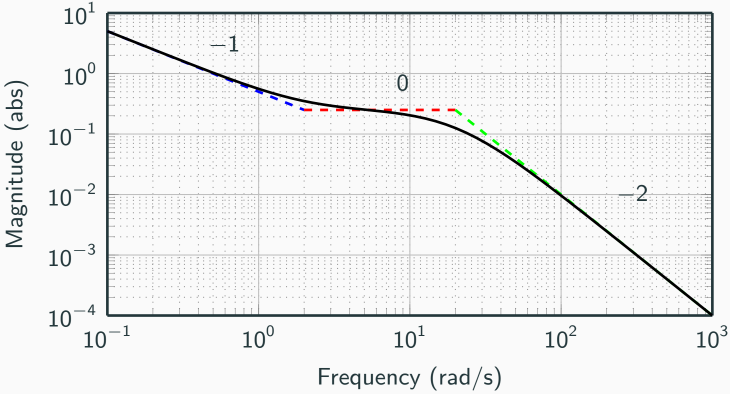

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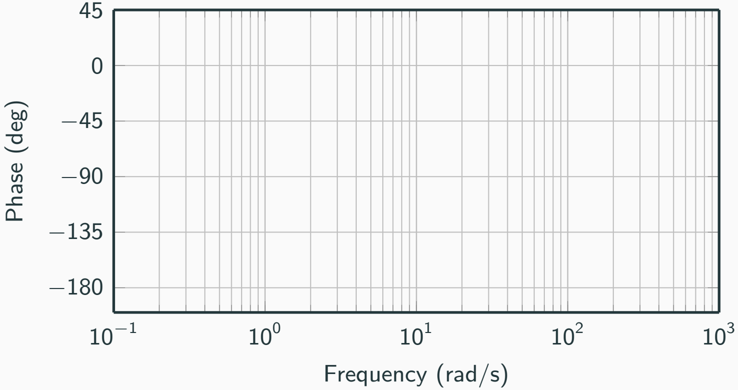

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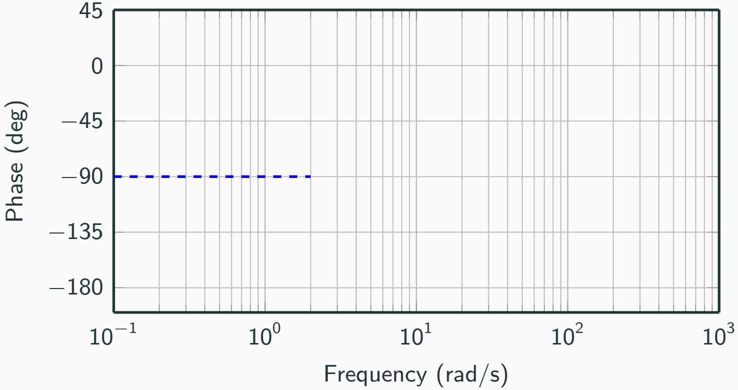

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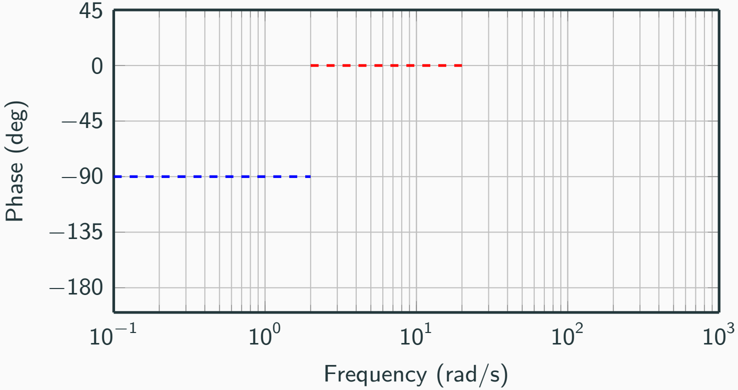

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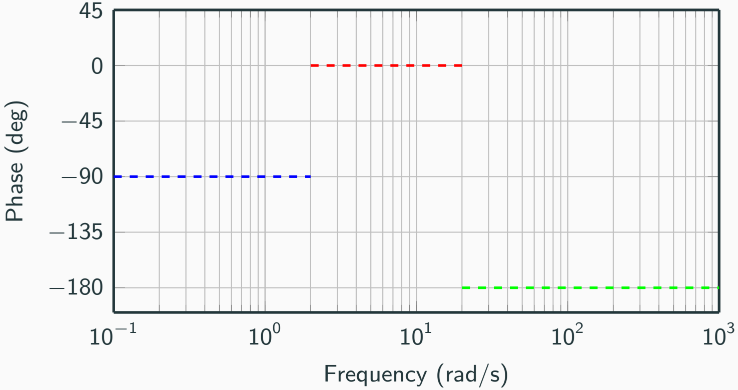

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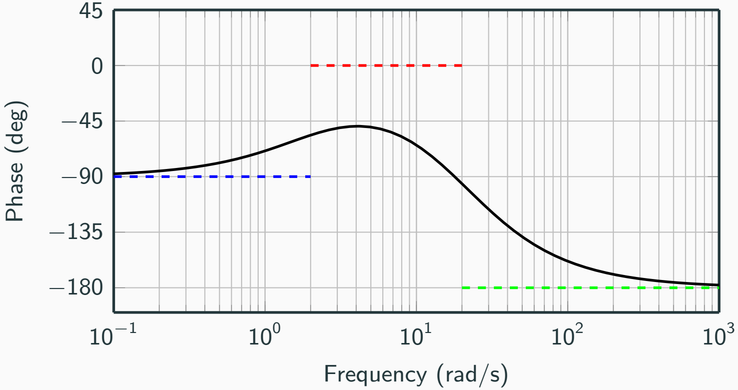
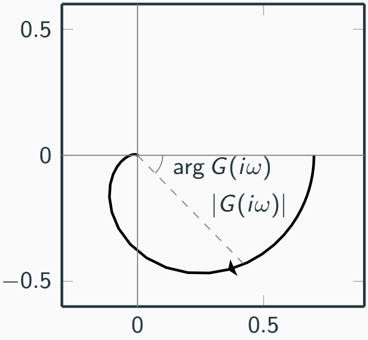


Nyquist Plot

By removing the frequency information, we can plot the transfer function in one plot instead of two



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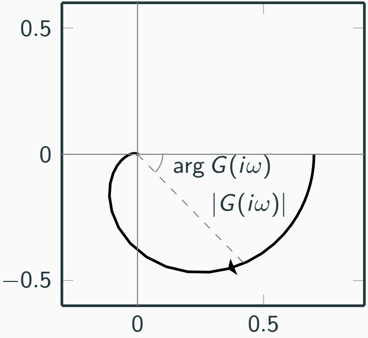
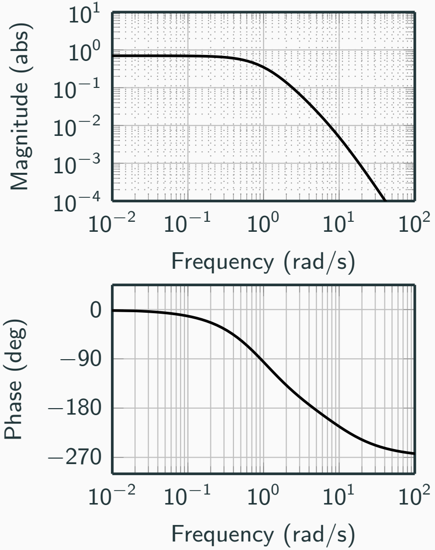


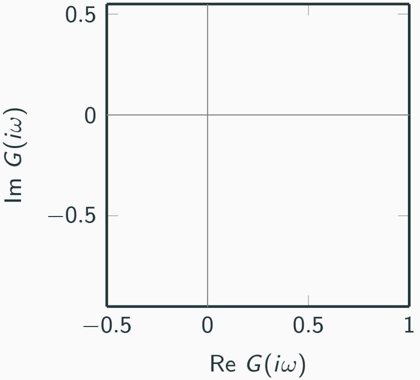
Split the transfer function into real and imaginary part:

$$G(s) = \frac{1}{1+s} \quad G(i\omega) = \frac{1}{1+i\omega} = \frac{1}{1+\omega^2} - i\frac{\omega}{1+\omega^2}$$

Is this the transfer function in the plot above?

From Bode Plot to Nyquist Plot





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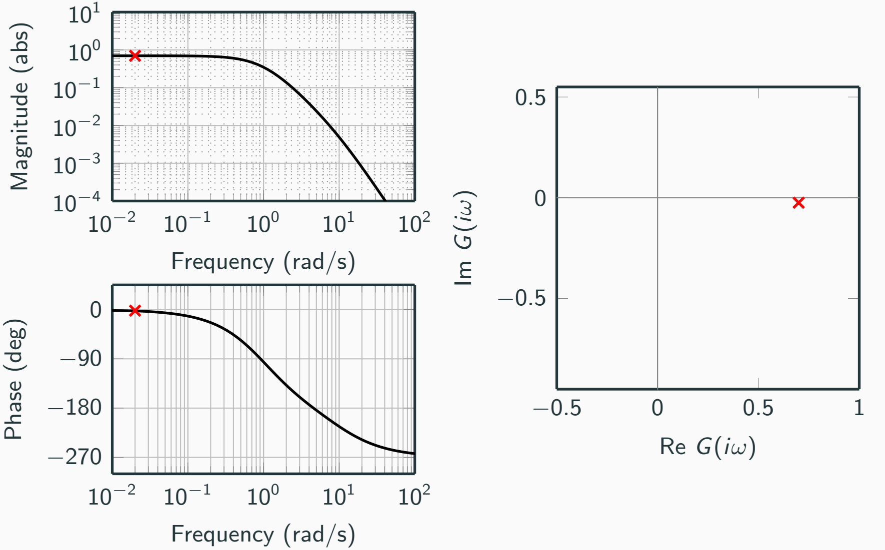

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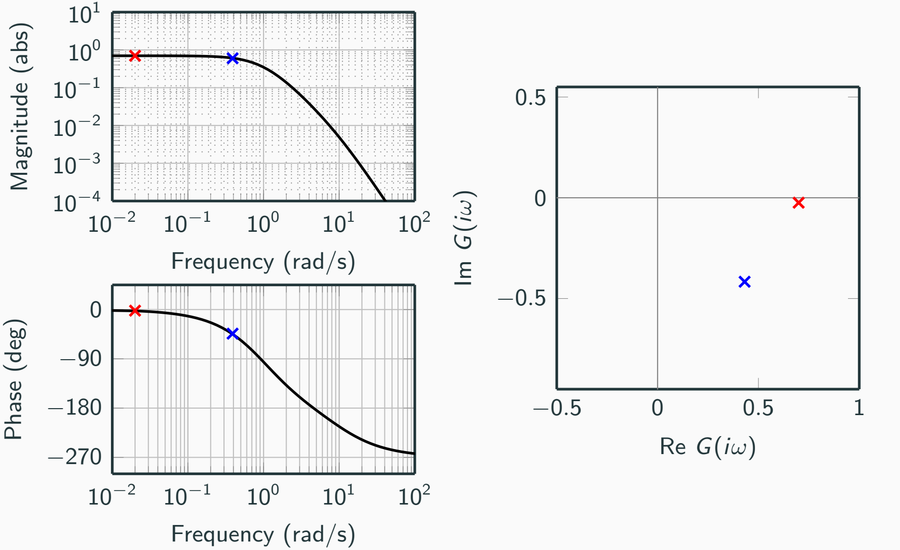

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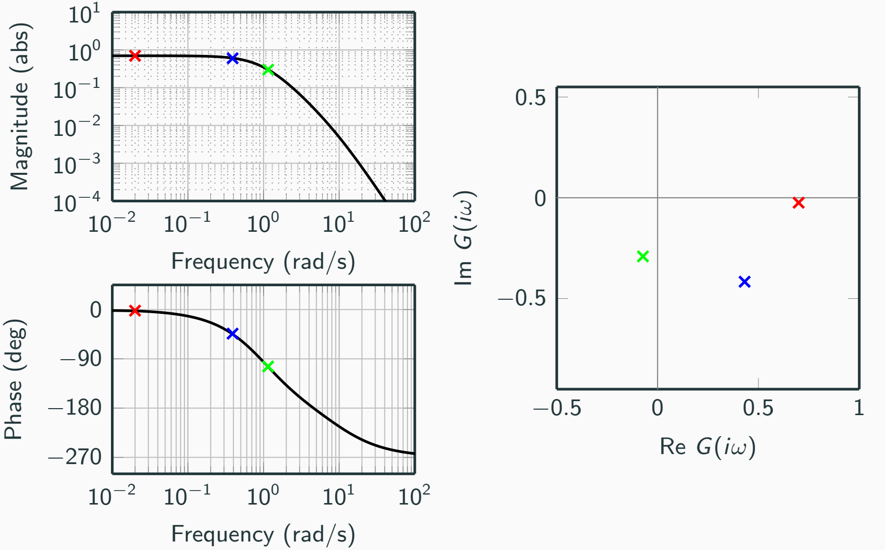

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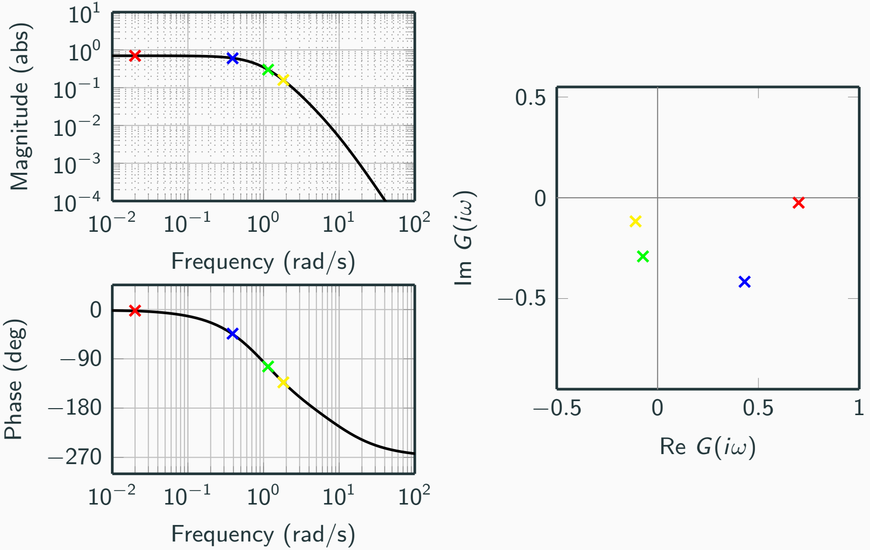

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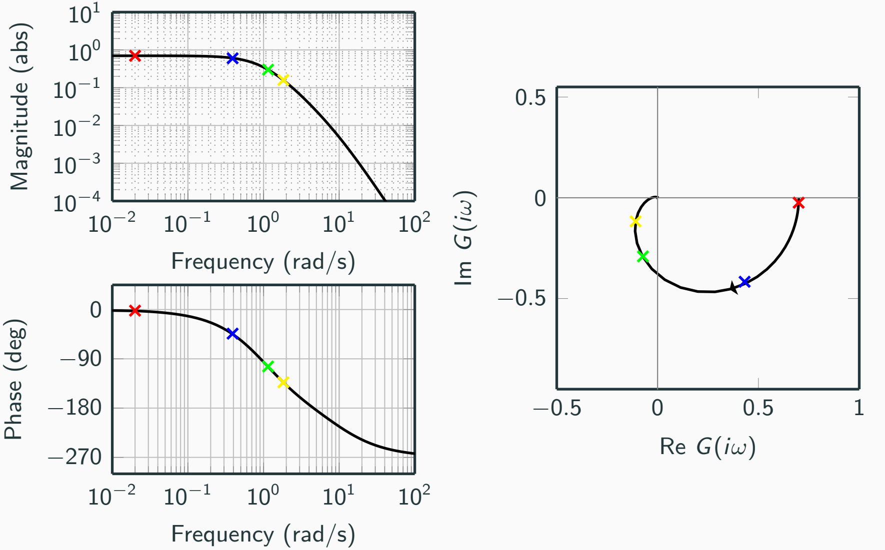
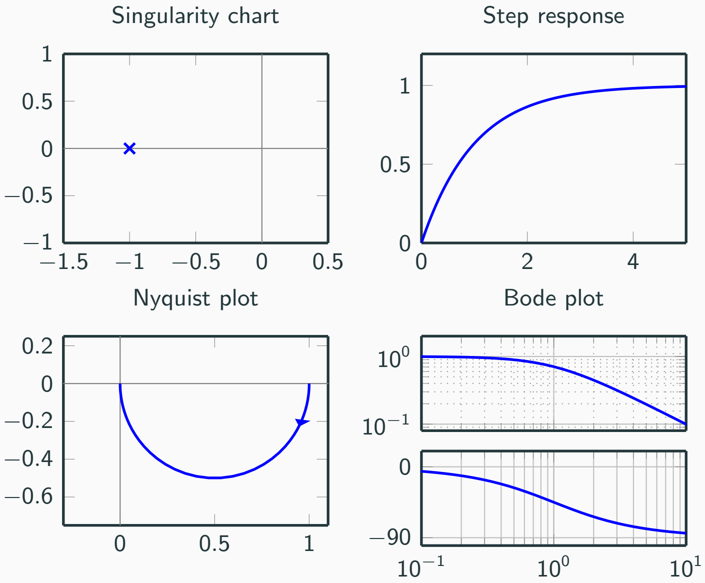
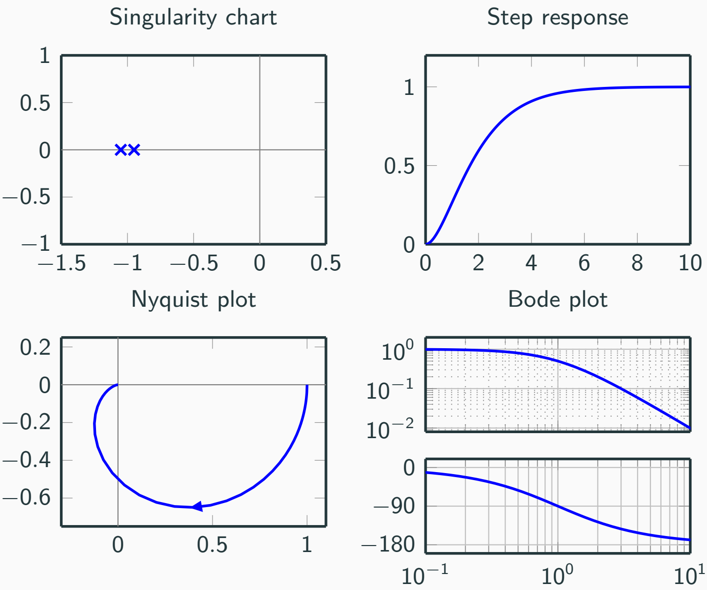


Relation between Model Descriptions

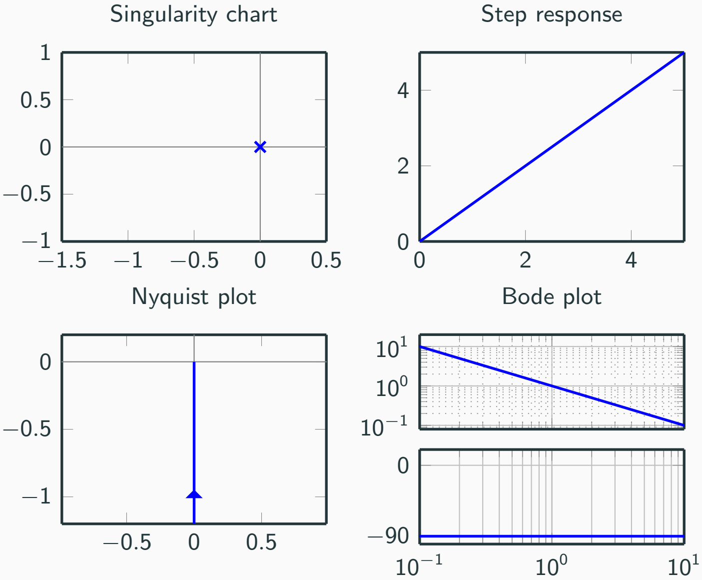
Single-capacitive Processes



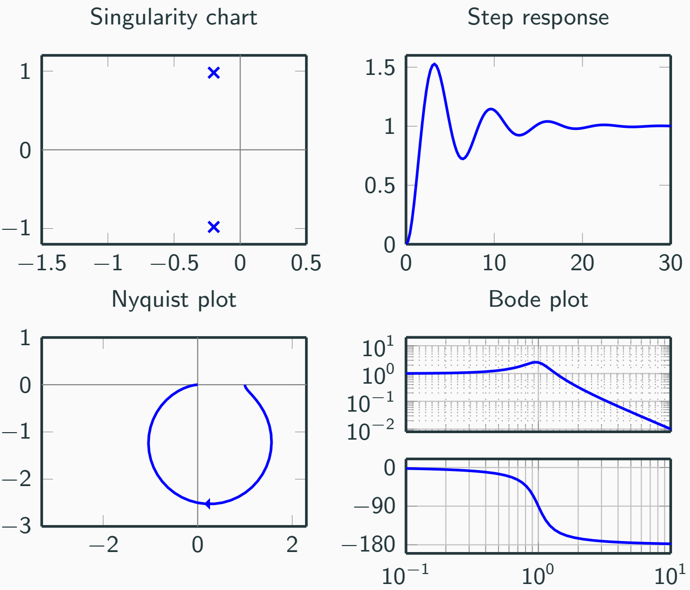
Multi-capacitive Processes



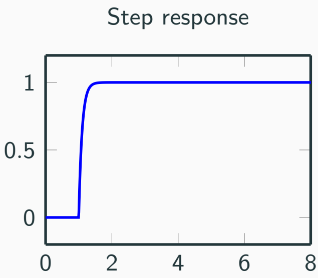
Integrating Processes

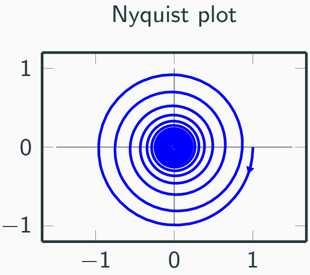


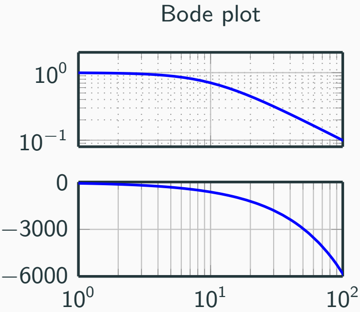
Oscillative Processes



Delay Processes







Process with Inverse Responses