- 1.
 - **a.** The Nernst equation for ion [i] is given by

$$E_i = \frac{\mathrm{RT}}{\mathrm{zF}} \ln\left(\frac{C_{out,i}}{C_{in,i}}\right)$$

where z - valence charge, C_{out} the ion concentration outside the cell, C_{in} the ion concentration inside the cell, R - thermodynamic gas constant, F - Faraday constant and T - temperature in Kelvin.

Given R = 8.31447 [J/mol·K], T = 273 + 25 [K] and $F = 9.648534 \cdot 10^4$ [C/mol] then RT/F = 0.0257 [V] or 25.7 [mV].

Using the Nernst equation with the given values of the inner/external concentrations as well as the valence charge results in $E_1 = 23$, $E_2 = -72$ and $E_3 = -12$ [mV].

b. A decrease in *T* results in the coefficient RT/F being smaller. Therefore a decrease in *T* results in a decrease in E_1 and an increase in E_2 and E_3 .

2.

a. The solution of $\dot{C} = -0.8C$ is given by $C(t) = C_0 e^{-0.8t}$. Solve $0.4C_0 = C_0 e^{-0.8T}$ for T to get the time.

$$0.4C_0 = C_0 e^{-0.8T}$$

$$0.4 = e^{-0.8T}$$

$$\ln(0.4) = -0.8T$$

$$T = \frac{\ln(0.4)}{-0.8} = 1.14$$
 hours ≈ 69 minutes.

b. The kinetics of the system is given by

$$\dot{C} = -0.8C + \frac{u}{V}$$

The transfer function of the system is

$$C(s) = \frac{1}{V} \frac{1}{s+0.8}$$

The static gain is C(0) = 1/(0.8V). And the constant dose that achieves the steady state is given by $u = C_{opt}/C(0)$.





or use (a, V_a) , and similarly, in each compartment.

b. Let $x = [a \ b \ c]^T$. Then the system can be written as

$$\dot{x} = \begin{bmatrix} -k_{ab} & k_{ba} & k_{ca} \\ k_{ab} & -(k_{ba} + k_{bc}) & 0 \\ 0 & k_{bc} & -k_{ca} \end{bmatrix}$$
$$y = \begin{bmatrix} 0 & 0 & 1/V_c \end{bmatrix} x.$$

c. It is easy to check that $\dot{a} + \dot{b} + \dot{c} = 0$. Thus a(t) + b(t) + c(t) = q, where q is some constant. Using the initial conditions we find that q = p.

4.

a. From the Nyquist plot it is clear that the amplitude margin is $A_m = 1/2$, and thus the larges K is 1/2.





c. Inserting $u = -Lx + l_r r$ gives $\dot{x} = (A - BL)X + Bl_r r$. The Laplace transform then gives $X(s) = (sI - A + BL)^{-1}Bl_r R(S)$. Thus the transfer function can then be found,

$$Y(s) = \underbrace{C(sI - A + BL)^{-1}Bl_r}_{G(S)} R(S)$$

d. Calculations gives

$$|sI - A + BL| = \det \begin{bmatrix} s - 1 + l_1 & l_2 \\ -2 & s - 1 \end{bmatrix} = s^2 + (l_1 - 2)s + 1 - l_1 + 2l_2$$

This is to be compared with $(s+1)^2 = s^2 + 2s + 1$. Identification of coefficients gives $l_1 = 4$ and $l_2 = 2$.

5.

- **a.** $\dot{x} = 0$ for x = 0 or $y = \alpha/\beta$ assuming $x \neq 0$. Likewise for \dot{y} we have that y = 0 or $x = \gamma/\delta$ assuming $y \neq 0$. Thus the two stational points that makes $\dot{x} = 0$ and $\dot{y} = 0$ is (0, 0) and $(\gamma/\delta, \alpha/\beta)$.
- **b.** Let

$$f = \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix}.$$

Then

$$\frac{\partial f}{\partial x}(x, y) = \begin{bmatrix} \alpha - \beta y \\ \delta y \end{bmatrix}, \quad \frac{\partial f}{\partial y}(x, y) = \begin{bmatrix} -\beta x \\ \delta x - \gamma \end{bmatrix}.$$

In the point of interest we have

$$\frac{\partial f}{\partial x}(x^0, y^0) = \begin{bmatrix} 0\\ \delta \frac{\alpha}{\beta} \end{bmatrix}, \quad \frac{\partial f}{\partial y}(x^0, y^0) = \begin{bmatrix} -\beta \frac{\gamma}{\delta}\\ 0 \end{bmatrix}.$$

Let $\Delta x = x - x^0$ and $\Delta y = y - y^0$. Then we have that

$$\begin{bmatrix} \Delta \dot{x} \\ \Delta \dot{y} \end{bmatrix} = \begin{bmatrix} 0 & -\beta \frac{\gamma}{\delta} \\ \delta \frac{\alpha}{\beta} & 0 \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta y \end{bmatrix}.$$

c. The poles of the systems are given by the solution to $s^2 + \alpha \gamma$. Thus the poles are given by $\pm i \sqrt{\alpha \gamma}$. The poles are on the imaginary axis and the linearized system is marginally stable.

a. Assuming steady state, the output is given by $y(t) = |G(3i)| \sin(3\omega t + \arg(G(3i)))$.

$$|G(3i)| = \frac{2}{\sqrt{9+9}} = \frac{2}{\sqrt{18}} = \frac{\sqrt{2}}{3}$$
$$\arg(G(3i) = -\arctan(1) = -\pi/4$$

It is also possible to use the method in the next subproblem.

b. We have that Y(s) = G(s)U(s) = 2/(s(s+3)) Using the collection of formulae we find that

$$y(t) = 2/3 \cdot (1 - e^{-3t})$$

c. The output of the first system can be found by

$$y_1(t) = \int_0^t h(t-\tau)u_2(\tau) \,\mathrm{d}\tau,$$

where \boldsymbol{h} is the impulse response of the linear system. Similarly for the second system

$$y_2(t) = \int_0^t h(t-\tau) u_2(\tau) \, \mathrm{d}\tau = \int_0^t h(t-\tau) 2u_1(\tau) \, \mathrm{d}\tau$$
$$= 2 \int_0^t h(t-\tau) u_1(\tau) \, \mathrm{d}\tau = 2y_1(t)$$

System B can not be linear as the responses from two different step sizes can not be related only by a positive scaling factor.

7. a - ii, b - iv, c- i, d-iii.

The step response in (a) have static gain 0.5.

The step response in (b) have a time delay.

The step response in (c) have static gain 1, but no time delay.

The step response in (d) is unstable (and have complex poles).

Tabell 1: Drug data for problem 1

Substrate concentration $[S]$ [units]	Reaction rate V [units/days]
0.5	0.12
1	0.27
2	0.33
4	0.58

8. Rewrite relationship as

$$\frac{1}{V} = \frac{K_m}{V_{max}} \frac{1}{[S]} + \frac{1}{V_{max}}.$$

Now, the parameters K_m/V_{max} and $1/V_{max}$ may be estimated as follows: Let the regressor matrix be

$$\Phi = \begin{pmatrix} 1 & 1/[S]_1 \\ 1 & 1/[S]_1 \\ 1 & 1/[S]_3 \\ 1 & 1/[S]_4 \end{pmatrix} = \begin{pmatrix} 1 & 2 \\ 1 & 1 \\ 1 & 0.5 \\ 1 & 0.25 \end{pmatrix}$$

where $[S]_i$ is the i-th value of [S] in Table 1. Denote

$$y = (1/V_1 \ 1/V_2 \ 1/V_3 \ 1/V_4)^T = (8.33 \ 3.70 \ 3.03 \ 1.73)^T$$

where V_i is the i-th value of V is Table 1. The least-squares solution is then

$$\begin{pmatrix} \frac{1}{\hat{V}_{max}} \\ \frac{\hat{K}_m}{V_{max}} \end{pmatrix} = \left(\Phi^T \Phi \right)^{-1} \Phi^T y = \begin{pmatrix} 0.77 \\ 3.66 \end{pmatrix}$$

which results in $\hat{V}_{max} = 1.30$ and $\hat{K}_m = 4.77$.

Good Luck!