

# Last week

- State Space Realizations (pp 139-150)
- $G(s)$ , denominator and numerator, poles and zeros
- Change of coordinates, diagonal and controllable form
- State-feedback
- Observers
- Feedback from estimated states
- Integral action by disturbance model

# Lecture 5

- Controllability – Existence of control signal
  - Which state directions can be controlled ?
- Observability – Determine state
  - Which state directions can not be seen?
- Kalman's decomposition theorem
- Cancelled dynamics  $\Leftrightarrow$  lack of controllability or observability

# Controllability

How should **controllability** be defined ?

Some (not used) alternatives:

By proper choice of control signal  $u$

- any state  $x_0$  can be made an equilibrium
- any state trajectory  $x(t)$  can be obtained
- any output trajectory  $y(t)$  can be obtained

The most fruitful definition has instead turned out to be the following

# Controllability

The state equation

$$\dot{x}(t) = Ax(t) + Bu(t), \quad x(0) = x_0$$

is called *controllable* if for any  $x_0$  and  $T > 0$ , there exists  $u(t)$  such that  $x(T) = 0$  (“Controllable to origin”)

Question: Is this equivalent to the following definition:

“for  $x_0 = 0$  and any  $x_1$  and  $T > 0$ , there exists  $u(t)$  such that  $x(T) = x_1$ ” (“Controllable from origin”)

The audience is thinking!

Hint:  $x(T) = e^{AT}x_0 + \int_0^T e^{A(T-t)}Bu(t)dt$

# Controllability Gramian

The matrix function

$$W(T) = \int_0^T e^{-At} B(t) B(t)^T e^{-A^T t} dt$$

is called the *controllability Gramian*.

A main result is the following

# Controllability Test

The following conditions are equivalent: We will not prove this (see link on home page).

- (i) The system  $\dot{x}(t) = Ax(t) + Bu(t)$  is controllable.
- (ii)  $\text{rank} [B \ AB \ A^2B \ \dots \ A^{n-1}B] = n$ .
- (iii)  $W(T)$  is invertible for any  $T > 0$
- (iv) For any  $\lambda \in \mathbf{C}$  we have  $\text{rank}[A - \lambda I \ B] = n$

The condition (iv) is called the PBH test (Popov-Belevitch-Hautus)

How much rank is lost in  $A - \lambda I$ , how much is saved by  $B$ ?

# Explicit construction of $u(t)$

If  $W(T)$  is invertible, then for any initial state  $x_0$ , the control signal

$$u(t) = -B^T e^{-A^T t} (W(T))^{-1} x_0$$

gives  $x(T) = 0$  (easy to check!). Hence the system is controllable.

## Another interpretation of $W(T)$

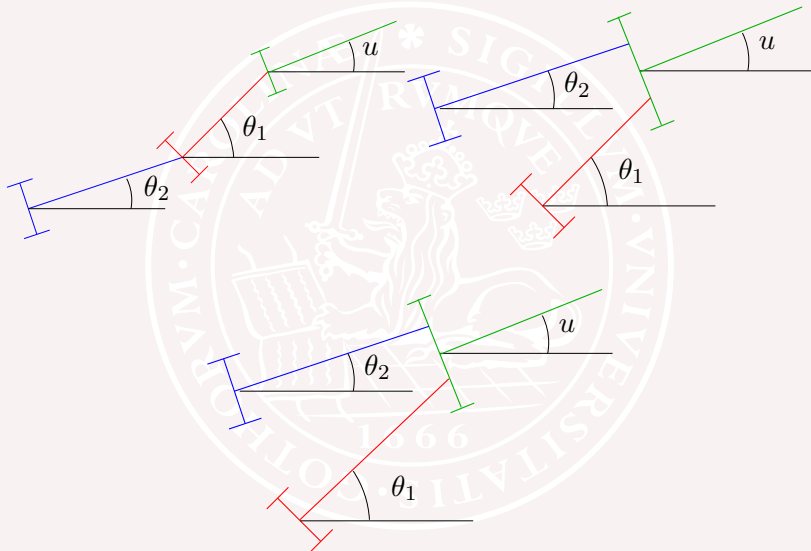
One can prove (using techniques from next lecture) that the minimal (squared) control energy, defined by  $\|u\|^2 := \int_0^T |u|^2 dt$ , needed to move from  $x(0) = x_0$  to  $x(T) = 0$  equals

$$x_0^T (W(T))^{-1} x_0$$

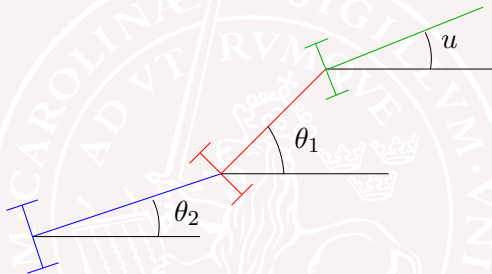
Gives nice understanding of which state directions are expensive to control



# Which trailer is controllable?

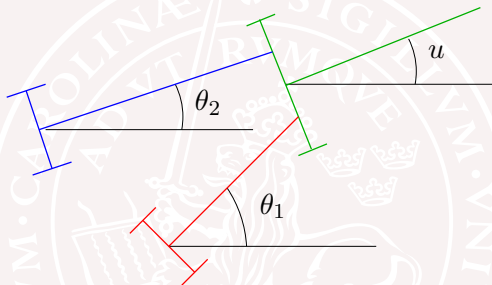


# Trailer 1



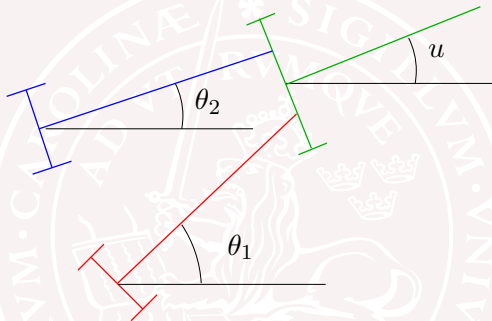
$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} + \begin{bmatrix} 2 \\ 0 \end{bmatrix} u$$

## Trailer 2



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u$$

## Trailer 3



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u$$

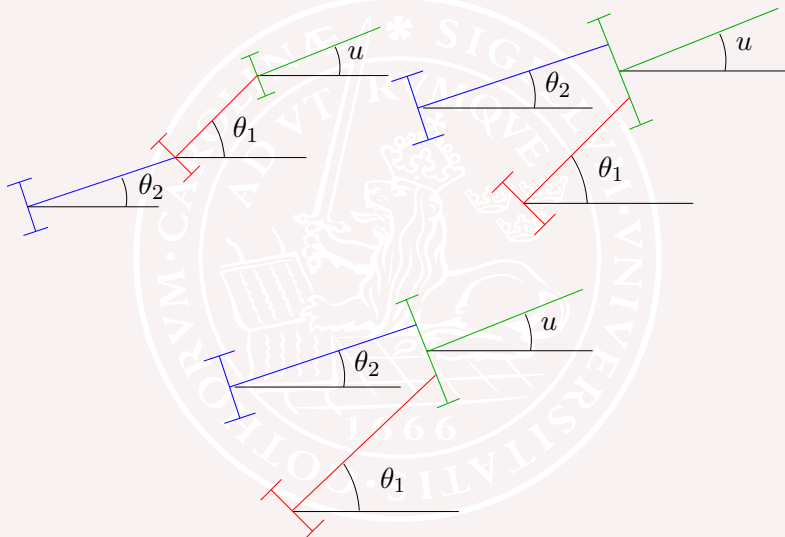
# Observability

The system

$$\begin{cases} \frac{dx}{dt} = Ax, & x(0) = x_0 \\ y = Cx \end{cases}$$

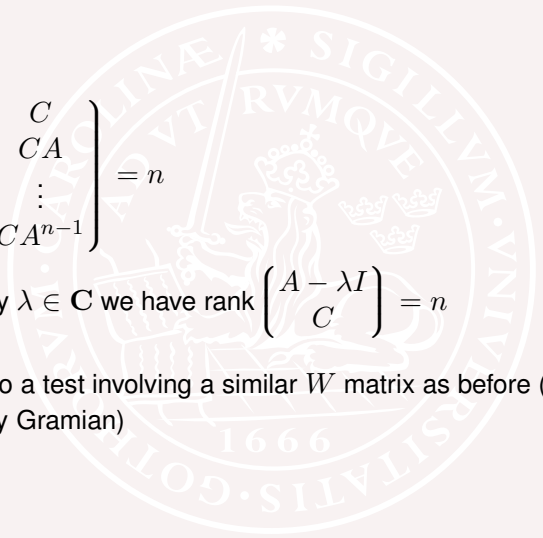
is called observable if  $x_0$  can be uniquely determined from  $y_{[0,T]}$  (for any  $T > 0$ )

# Which trailer is observable?



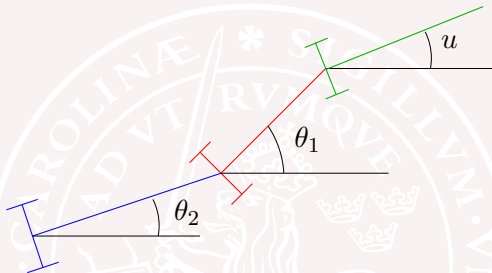
Which trailer is observable if  $y = \theta_1$ ? If  $y = \theta_2$ ?

# Observability Criteria

- 
- (i)  $\text{rank} \begin{pmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{pmatrix} = n$
- (ii) For any  $\lambda \in \mathbf{C}$  we have  $\text{rank} \begin{pmatrix} A - \lambda I \\ C \end{pmatrix} = n$

There is also a test involving a similar  $W$  matrix as before (called observability Gramian)

# Trailer 1

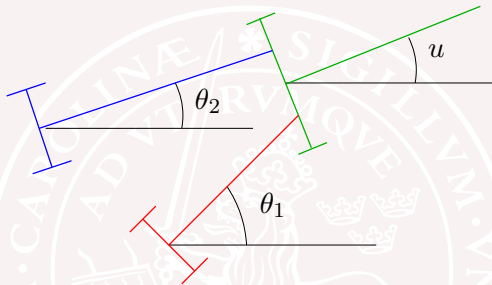


$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$

$$y = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$



## Trailer 2



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$
$$y = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$

# Controllability – state transformation

Theorem:

If the system is noncontrollable, say  $\text{rank}(\mathcal{C}) = q < n$ , then there is a state transformation  $x = Vz$  so that in the new state coordinates

$$AV = V \begin{pmatrix} \tilde{A}_{11} & \tilde{A}_{12} \\ 0 & \tilde{A}_{22} \end{pmatrix} \text{ and } B = V \begin{pmatrix} \tilde{B}_1 \\ 0 \end{pmatrix},$$

$(\tilde{A}_{11}, \tilde{B}_1)$  controllable subsystem,  $q \times q$

# Observability – state transformation

Theorem:

If the system is non-observable, say  $\text{rank}(\mathcal{O}) = q < n$ , then there is a state transformation so that in the new state coordinates

$$AV = V \begin{pmatrix} \tilde{A}_{11} & 0 \\ \tilde{A}_{21} & \tilde{A}_{22} \end{pmatrix} \text{ och } CV = \begin{pmatrix} \tilde{C}_1 & 0 \end{pmatrix},$$

$(\tilde{A}_{11}, \tilde{C}_1)$  observable subsystem,  $q \times q$

# Kalman's decomposition theorem

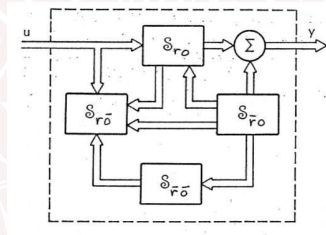
With a state transformation that splits the controllable subspace (and its complement) into nonobservable subspace and complement we get the system on a nice form

$$\frac{dx}{dt} = \begin{pmatrix} A_{11} & 0 & A_{13} & 0 \\ A_{21} & A_{22} & A_{23} & A_{24} \\ 0 & 0 & A_{33} & 0 \\ 0 & 0 & A_{43} & A_{44} \end{pmatrix} x + \begin{pmatrix} B_1 \\ B_2 \\ 0 \\ 0 \end{pmatrix} u$$
$$y = \begin{pmatrix} C_1 & 0 & C_2 & 0 \end{pmatrix} x$$

$$G(s) = C_1(sI - A_{11})^{-1}B_1$$

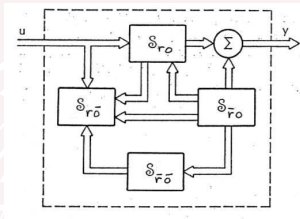
Illustrates what subparts of the system that influences the input-output behavior

# Kalman's decomposition theorem

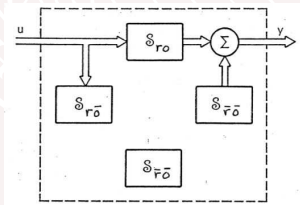


The audience is thinking: What blocks in this figure correspond to parts 1,2,3,4 on the previous slide?

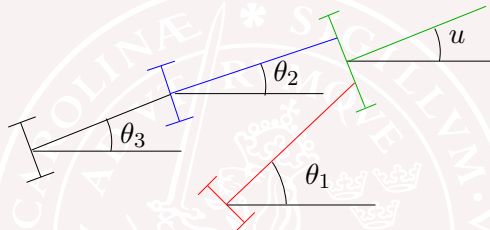
# Kalman's decomposition theorem



If no common eigenvalues between any two blocks on the diagonal, then corresponding off-diagonal blocks can be eliminated by changed choice of the complementing spaces. Simplifies picture further



## Trailer 4



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 2 & -2 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix} u, \quad y = \begin{bmatrix} 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix}$$

What does the decomposition theorem say when  $y = \theta_2$ ? What block is then missing?

## Trailer 4 after coordinate change

$$\begin{bmatrix} \dot{\theta}_2 \\ \dot{\theta}_3 \\ \dot{\theta}_1 - \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 \\ 2 & -2 & 0 \\ 0 & 0 & -1 \end{bmatrix} \begin{bmatrix} \theta_2 \\ \theta_3 \\ \theta_1 - \theta_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} u$$
$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} \theta_2 \\ \theta_3 \\ \theta_1 - \theta_2 \end{bmatrix}$$

controllable and observable subsystem:  $\theta_2$



# Zeros and state feedback

Remember: State-feedback does not change zeros.

Choose state feedback  $L$  that gives a pole in  $\lambda$ .

If the mode  $x_0 e^{\lambda t}$  now becomes non-observable

$$\begin{pmatrix} A - BL - \lambda I \\ C \end{pmatrix} x_0 = 0$$

then actually  $\lambda$  was a zero to the system:

$$\begin{pmatrix} A - \lambda I & B \\ C & 0 \end{pmatrix} \begin{pmatrix} x_0 \\ u_0 \end{pmatrix} = 0$$

Corresponds to cancellation of the factor  $s - \lambda$  in

$$G(s) = C(sI - A + BL)^{-1} B l_r$$

## Bonus: Series Connection SISO

Given two systems  $n_i(s)/d_i(s) = c_i(sI - A_i)^{-1}b_i$ ,  $i = 1, 2$

Then the series connection  $\frac{n_2(s)}{d_2(s)} \frac{n_1(s)}{d_1(s)}$  is

- uncontrollable  $\iff$  there is  $\lambda$  so  $n_1(\lambda) = d_2(\lambda) = 0$
- unobservable  $\iff$  there is  $z$  so  $n_2(\lambda) = d_1(\lambda) = 0$

Proof:

Controllable, check when rank  $\begin{bmatrix} \lambda I - A_1 & 0 & b_1 \\ -b_2 c_1 & \lambda I - A_2 & 0 \end{bmatrix} \leq n$

Observable, check when rank  $\begin{bmatrix} \lambda I - A_1 & 0 \\ -b_2 c_1 & \lambda I - A_2 \\ 0 & c_2 \end{bmatrix} \leq n$

# Cancellation in series connections

Example

$$Y(s) = \frac{s+3}{s-1} \cdot \frac{s-1}{s+2} U(s)$$

Loss of controllability of an unstable mode. Bad.

Example

$$Y(s) = \frac{s-1}{s+2} \cdot \frac{s+3}{s-1} U(s)$$

Loss of observability of an unstable mode. Also bad.

# Summary

- Controllability - criteria
- Observability - criteria
- Kalman's decomposition
- Cancelled dynamics  $\Leftrightarrow$  lack of controllability or observability