

Last week

- State Space Realizations (pp 139-150)
- $G(s)$, denominator and numerator, poles and zeros
- Change of coordinates, diagonal and controllable form
- State-feedback
- Observers
- Feedback from estimated states
- Integral action by disturbance model

Lecture 5

- Controllability – Existence of control signal
- Which state directions can be controlled ?
- Observability – Determine state
- Which state directions can not be seen?

- Kalman's decomposition theorem
- Non controllability of the estimation error
- Zeros and state feedback
- Cancellation with series connections

Controllability

How should **controllability** be defined ?

Some (not used) alternatives:

By proper choice of control signal u

- any state x_0 can be made an equilibrium
- any state trajectory $x(t)$ can be obtained
- any output trajectory $y(t)$ can be obtained

The most fruitful definition has instead turned out to be the following

Controllability

The state equation

$$\dot{x}(t) = Ax(t) + Bu(t), \quad x(0) = x_0$$

is called *controllable* if for any x_0 and $T > 0$, there exists $u(t)$ such that $x(T) = 0$ ("Controllable to origin")

Question: Is this equivalent to the following definition:

"for $x_0 = 0$ and any x_1 and $T > 0$, there exists $u(t)$ such that $x(T) = x_1$ " ("Controllable from origin")

The audience is thinking!

Hint: $x(T) = e^{AT}x_0 + \int_0^T e^{A(T-t)}Bu(t)dt$

Controllability Gramian

The matrix function

$$W(T) = \int_0^T e^{-At} B(t) B(t)^T e^{-A^T t} dt$$

is called the *controllability Gramian*.

A main result is the following

Controllability Test

The following conditions are equivalent: We will not prove this (see link on home page).

- (i) The system $\dot{x}(t) = Ax(t) + Bu(t)$ is controllable.
- (ii) $\text{rank} [B \ AB \ A^2B \ \dots \ A^{n-1}B] = n$.
- (iii) $W(T)$ is invertible for any $T > 0$
- (iv) For any $\lambda \in \mathbf{C}$ we have $\text{rank}[A - \lambda I \ B] = n$

The condition (iv) is called the PBH test (Popov-Belevitch-Hautus)

How much rank is lost in $A - \lambda I$, how much is saved by B ?

Explicit construction of $u(t)$

If $W(T)$ is invertible, then for any initial state x_0 , the control signal

$$u(t) = -B^T e^{-A^T t} (W(T))^{-1} x_0$$

gives $x(T) = 0$ (easy to check!). Hence the system is controllable.

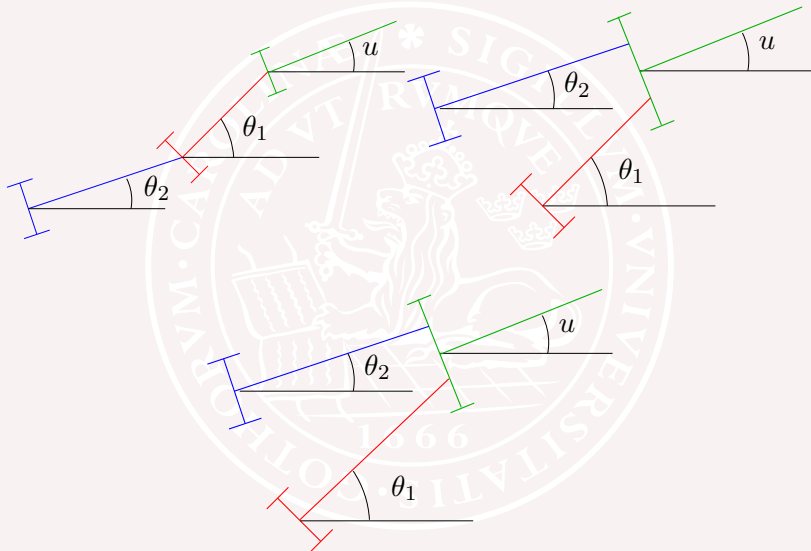
Another interpretation of $W(T)$

One can prove (using techniques from next lecture) that the minimal (squared) control energy, defined by $\|u\|^2 := \int_0^T |u|^2 dt$, needed to move from $x(0) = x_0$ to $x(T) = 0$ equals

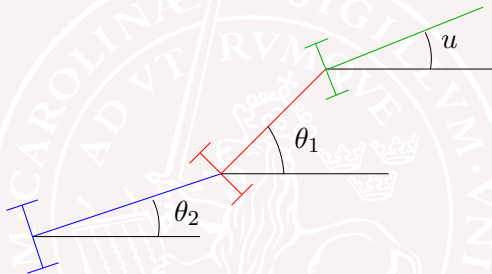
$$x_0^T (W(T))^{-1} x_0$$

Gives nice understanding of which state directions are expensive to control

Which trailer is controllable?

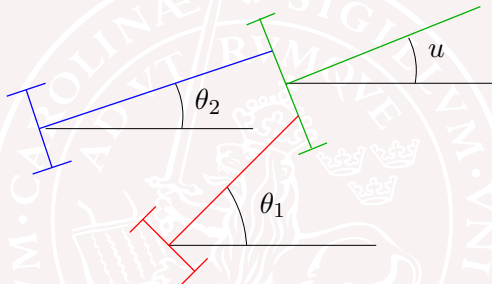


Trailer 1



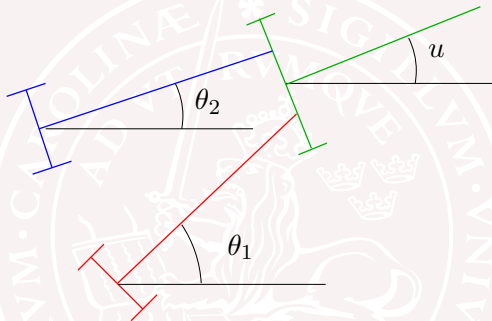
$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} + \begin{bmatrix} 2 \\ 0 \end{bmatrix} u$$

Trailer 2



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u$$

Trailer 3



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u$$

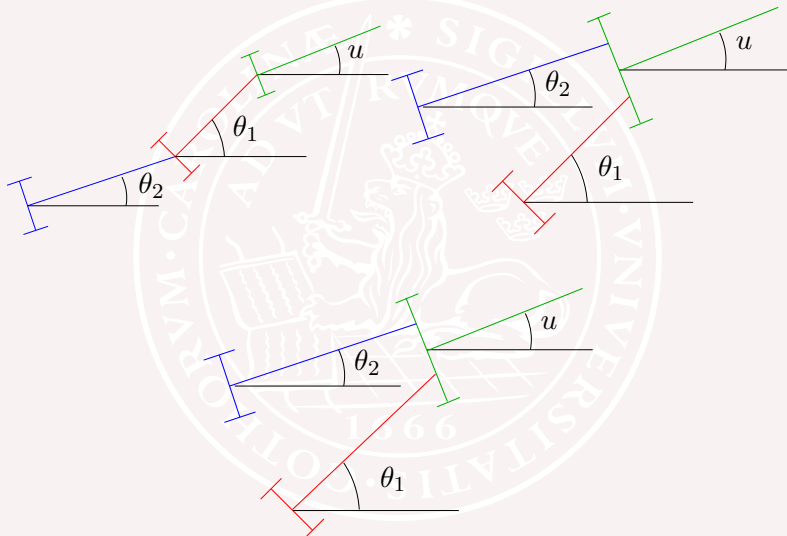
Observability

The system

$$\begin{cases} \frac{dx}{dt} = Ax, & x(0) = x_0 \\ y = Cx \end{cases}$$

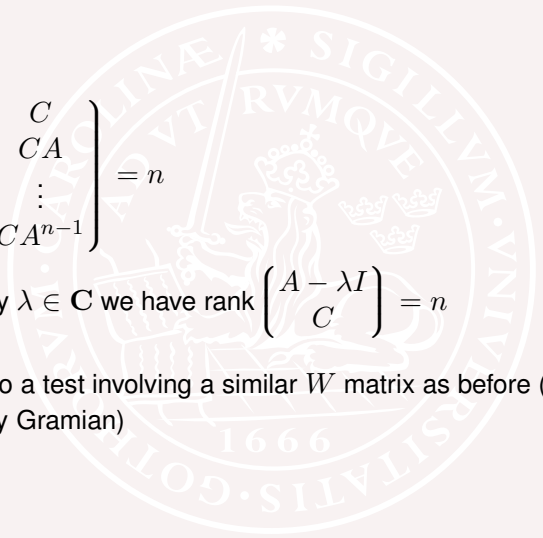
is called observable if x_0 can be uniquely determined from $y_{[0,T]}$ (for any $T > 0$)

Which trailer is observable?



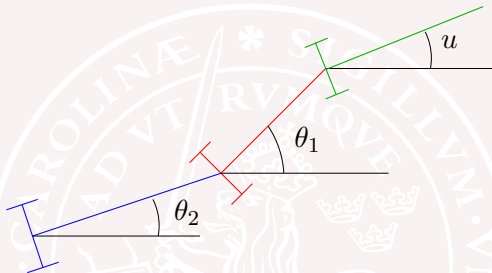
Which trailer is observable if $y = \theta_1$? If $y = \theta_2$?

Observability Criteria

- 
- (i) $\text{rank} \begin{pmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{pmatrix} = n$
- (ii) For any $\lambda \in \mathbf{C}$ we have $\text{rank} \begin{pmatrix} A - \lambda I \\ C \end{pmatrix} = n$

There is also a test involving a similar W matrix as before (called observability Gramian)

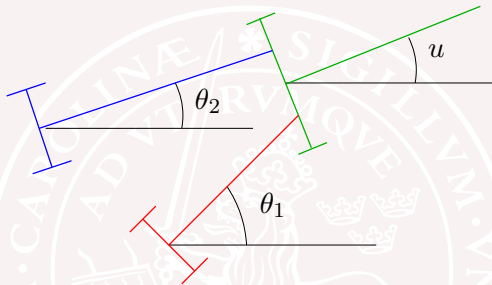
Trailer 1



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$

$$y = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$

Trailer 2



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix} \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$
$$y = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$

Controllability – state transformation

Theorem:

If the system is noncontrollable, say $\text{rank}(\mathcal{C}) = q < n$, then there is a state transformation $x = Vz$ so that in the new state coordinates

$$AV = V \begin{pmatrix} \tilde{A}_{11} & \tilde{A}_{12} \\ 0 & \tilde{A}_{22} \end{pmatrix} \text{ and } B = V \begin{pmatrix} \tilde{B}_1 \\ 0 \end{pmatrix},$$

$(\tilde{A}_{11}, \tilde{B}_1)$ controllable subsystem, $q \times q$

Observability – state transformation

Theorem:

If the system is non-observable, say $\text{rank}(\mathcal{O}) = q < n$, then there is a state transformation so that in the new state coordinates

$$AV = V \begin{pmatrix} \tilde{A}_{11} & 0 \\ \tilde{A}_{21} & \tilde{A}_{22} \end{pmatrix} \text{ och } CV = \begin{pmatrix} \tilde{C}_1 & 0 \end{pmatrix},$$

$(\tilde{A}_{11}, \tilde{C}_1)$ observable subsystem, $q \times q$

Kalman's decomposition theorem

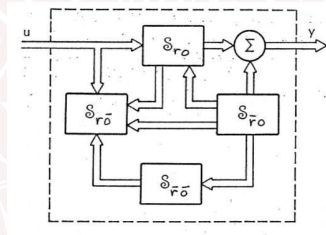
With a state transformation that splits the controllable subspace (and its complement) into nonobservable subspace and complement we get the system on a nice form

$$\frac{dx}{dt} = \begin{pmatrix} A_{11} & 0 & A_{13} & 0 \\ A_{21} & A_{22} & A_{23} & A_{24} \\ 0 & 0 & A_{33} & 0 \\ 0 & 0 & A_{43} & A_{44} \end{pmatrix} x + \begin{pmatrix} B_1 \\ B_2 \\ 0 \\ 0 \end{pmatrix} u$$
$$y = \begin{pmatrix} C_1 & 0 & C_2 & 0 \end{pmatrix} x$$

$$G(s) = C_1(sI - A_{11})^{-1}B_1$$

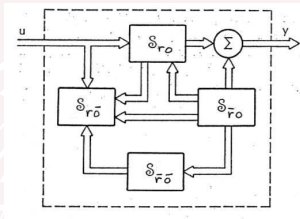
Illustrates what subparts of the system that influences the input-output behavior

Kalman's decomposition theorem

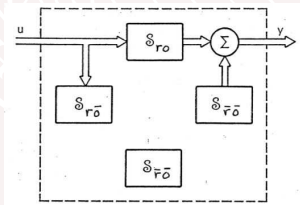


The audience is thinking: What blocks in this figure correspond to parts 1,2,3,4 on the previous slide?

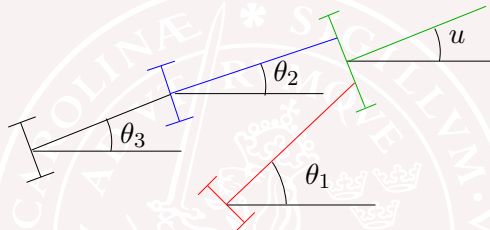
Kalman's decomposition theorem



If no common eigenvalues between two block on the diagonal, then corresponding off-diagonal blocks can be eliminated by changed choice of the complementing spaces. Simplifies picture further



Trailer 4



$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 2 & -2 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix}, \quad y = \begin{bmatrix} 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix}$$

What does the decomposition theorem say when $y = \theta_2$? What block is then missing?

Trailer 4 after coordinate change

$$\begin{bmatrix} \dot{\theta}_2 \\ \dot{\theta}_3 \\ \dot{\theta}_1 - \dot{\theta}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 \\ 2 & -2 & 0 \\ 0 & 0 & -1 \end{bmatrix} \begin{bmatrix} \theta_2 \\ \theta_3 \\ \theta_1 - \theta_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} u$$
$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} \theta_2 \\ \theta_3 \\ \theta_1 - \theta_2 \end{bmatrix}$$

controllable and observable subsystem: θ_2

Zeros and state feedback

Remember: State-feedback does not change zeros.

Choose state feedback L that gives a pole in λ .

If the mode $x_0 e^{\lambda t}$ now becomes non-observable

$$\begin{pmatrix} A - BL - \lambda I \\ C \end{pmatrix} x_0 = 0$$

then actually λ was a zero to the system:

$$\begin{pmatrix} A - \lambda I & B \\ C & 0 \end{pmatrix} \begin{pmatrix} x_0 \\ u_0 \end{pmatrix} = 0$$

Corresponds to cancellation of the factor $s - \lambda$ in

$$G(s) = C(sI - A + BL)^{-1} B l_r$$

Bonus: Series Connection SISO

Given two systems $n_i(s)/d_i(s) = c_i(sI - A_i)^{-1}b_i$, $i = 1, 2$

Then the series connection $\frac{n_2(s)}{d_2(s)} \frac{n_1(s)}{d_1(s)}$ is

- uncontrollable \iff there is λ so $n_1(\lambda) = d_2(\lambda) = 0$
- unobservable \iff there is z so $n_2(\lambda) = d_1(\lambda) = 0$

Proof:

Controllable, check when rank $\begin{bmatrix} \lambda I - A_1 & 0 & b_1 \\ -b_2 c_1 & \lambda I - A_2 & 0 \end{bmatrix} \leq n$

Observable, check when rank $\begin{bmatrix} \lambda I - A_1 & 0 \\ -b_2 c_1 & \lambda I - A_2 \\ 0 & c_2 \end{bmatrix} \leq n$

Cancellation in series connections

Example

$$Y(s) = \frac{s+3}{s-1} \cdot \frac{s-1}{s+2} U(s)$$

Loss of controllability of an unstable mode. Bad.

Example

$$Y(s) = \frac{s-1}{s+2} \cdot \frac{s+3}{s-1} U(s)$$

Loss of observability of an unstable mode. Also bad.

Summary

- Controllability - criteria
- Observability - criteria
- Kalman's decomposition
- Cancelled dynamics \Leftrightarrow lack of controllability or observability